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Evaluation of a new packing material for H₂S removed by biofiltration

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This study aims to evaluate the feasibility of using a new packing material (UP20) in treating H₂S. Three identical laboratory-scale biofilters, filled with, respectively, UP20 alone, pine bark, and a configuration made of two layers of pozzolan/UP20 (80/20, v/v), were used for critical comparison. Various concentrations of H₂S (up to 100 ppmv) were used to determine the optimum biofilter performances. The superficial velocity of the polluted gas on each biofilter was 65 m h^{-1} (0.018 m s⁻¹; gas flow rate 0.5 N m³ h⁻¹) corresponding to an empty bed residence time of 57 s. Changes in elimination capacity, removal efficiency, moisture content, temperature and pH were tracked during 95 days. The pressure drops along each biofilter were also measured by varying the gas flow rate from 0.5 to 4 N m³ h⁻¹. After 63 days of operation, the loading rate was significantly increased to 10 g m⁻³ h⁻¹ and the UP20 biofilter retained a removal efficiency of more than 93%, indicating a strong ability to stimulate microbial activity (compared to 69% for the pine bark biofilter and 74% for the biofilter filled with a configuration of two layers of pozzolan/UP20). A Michaelis–Menten type equation was applied and the maximum removal rate (V_m) and saturation constant (K_s) were calculated. V_m was evaluated at 35 g H₂S $m_{\text{biofilter}}^{-3}$ h⁻¹ for UP20 (14 and 15 g H₂S $m_{\text{biofilter}}^{-3}$ h⁻¹ for pine bark and pozzolan/UP20, respectively). The saturation constant K_s was 70 ppmv for UP20 (18 ppmv for pine bark and 20 ppmv for pozzolan/UP20) indicating that the new packing material will be effective in treating large pollutant concentrations. At low concentrations of pollutant, the results suggest that a biofilter with a configuration of two layers of pozzolan/UP20 is the most suitable choice for treating H₂S.

1. Introduction

Biofiltration is currently the most used biological gas treatment technology. It involves microorganisms immobilized in the form of a biofilm on a porous carrier such as peat, soil, compost, synthetic substances or combinations of these. Biofiltration has gained worldwide acceptance as an economical air pollution control technology for the treatment of gas streams containing low concentrations of biodegradable volatile organic and inorganic compounds [1]. The pollutant substances are transferred from the air flow to the biofilm developing on the organic substrate where they are degraded by microorganisms. The treatment of H_2S in a biofilter leads to sulphate, thiosulphate or elemental sulphur production according to the operating conditions and to the microorganisms involved [2–4]. Although the microbiological aspects are of major importance in understanding the operating mode of microorganisms in biofiltration, the heart of the process could be the packing material, which must provide a favourable environment in terms of moisture, temperature, pH, nutrients and oxygen supply [4–6]. An ideal packing material should have the following characteristics [7]: (i) suitable particle size, void fraction and specific surface area, which indicate the surface available for biomass attachment; (ii) high nutritive capacity; (iii) high moisture retention capacity; (iv) high buffering capacity avoiding large pH fluctuations and (v) mechanically resistant, chemically inert and stable.

The most common packing materials are peat, soil and compost followed by wood bark, sugarcane bagasse [8] and peanut shells [5]. However, these materials lead to bed compression causing pressure drops and thus decreasing biofilter efficiency. Organic media also need to be replaced after 3–5 years, and they are difficult to regenerate [9]. Inorganic materials have also been studied. Metal oxides like porous ceramics, calcinated cristobalite [10] or perlite [11] have been used. However, their cost remains high and they do not provide any nutrients to the biomass. As for the geometrical characteristics of the material, it has been demonstrated that the best carrier must have a cylindrical shape [12,13].

Consequently, a new packing material, a cylindrical-shaped extrudate called UP20 (containing mainly calcium carbonate and an organic binder), has been developed in our laboratory for the treat-

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Fig. 1. Packing materials used.

ment of H₂S. The formulation of several new materials has been described in a previous work [7] and it has been demonstrated that the newly formulated UP20 offers a real advantage to the process at relatively high pollution concentration by providing both nutrients for the biomass and a buffering effect.

The main objective of this work is to investigate the removal of H₂S as a single pollutant in a biofilter packed with the new UP20 in terms of elimination capacity, removal efficiency, pH changes and pressure drops. The results are compared with two biofilters, one packed with pine bark and the other with a configuration made of pozzolan and UP20 stratified in two layers (80/20, v/v). Moreover, the kinetic constants are evaluated using a suitable mathematical model

2. Materials and methods

2.1. Packing materials

UP20 material contains CH₄N₂O, H₃PO₄, CaCO₃ (C/N/P molar ratio: 100/5/1) and an organic binder (20% in mass) from Elotex industry (it is a white powder commonly used in the building industry and mainly constituted of ethylene and vinyl acetate). UP20 has been extruded in a cylindrical shape according to the following procedure: first, the dry salt powders have been mixed in a container by shaking for 15 min; second, the organic binder has been introduced into water; third, the mixture of salt powders has been added to water. The amount of water was 66% of the dry salt mixture weight. Extrusion has been performed with a meat mincer and the granules have been dried at 50°C for 20h [7]. The dimensions of granules (Fig. 1) are 7 mm in diameter and 15 mm in length (average length calculated from a sample of 50 granules). Two others packing materials have been used for performance comparisons: pine bark and pozzolan (Fig. 1). Pine bark has been chosen for its good physical properties (low bed density) and very low price. It seemed interesting to compare the results obtained on the UP20 with those obtained on an organic material in operating conditions. Pozzolan is a volcanic siliceous rock, inert and relatively cheap. Its mechanical characteristics are very favourable for water filtration processes (low density, large porosity, large specific surface area and low ability to retain water). Pozzolan used in this study was mainly composed with SiO₂ (44%), Al₂O₃ (15%), Fe₂O₃ (15%) and CaO (10%) and appeared as irregular spherical beads with diameters ranging from 5 to 10 mm (Fig. 1). Pozzolan has been chosen in order to study a composite biofilter filled with an "ideal packing material": an inert mineral material having good mechanical properties in association with a layer of UP20 providing the nutrients to the biomass.

Table 1 presents some characteristics of the three packing materials. The specific surface area (a_{vs}) and the density (ρ_{hulk}) were measured by mercury intrusion porosimetry (Micromeritics AutoPore IV 9500). It appears that the specific surface area of UP20 is the lowest: $705 \text{ m}^2 \text{ m}^{-3}$ against $1120 \text{ m}^2 \text{ m}^{-3}$ for pine bark and 1060 m² m⁻³ for pozzolan. Herrygers et al. [14] indicated that the specific surface area of filtering materials lies typically between 300 and 1000 m² m⁻³ indicating that UP20 has a sufficiently high specific surface area to be a medium for biofiltration. Table 1 also indicates the maximum H₂S sorption capacities for the three biofilter beds in dry conditions [7]. It is clear that UP20 and pozzolan have much lower H₂S sorption capacities than pine bark (110 mg kg⁻¹). In comparison, Barona et al. [15] obtained a value close to 370 mg kg⁻¹ for activated carbon. Consequently, the non-biological removal of the pollutant will be very low and it is assumed that H₂S will be directly transferred from the gas phase to the water phase in order to be transformed by the microorganisms.

2.2. Experimental setup

The experimental equipment used in this work is shown in Fig. 2. Three biofilters were constructed with plastic cylinders (1.5 m in height and 0.1 m in diameter). The first biofilter was filled with 4.95 kg of UP20 (H=1m; white material on the left column in Fig. 2a); the second biofilter was packed with 1.55 kg of pine bark (1 m) and the third biofilter was filled with 5.06 kg of pozzolan (0.8 m) topped with 1.02 kg of UP20 (0.2 m; Fig. 2a). For each biofilter, the polluted air was introduced into the bottom of the column. The gas flow to be treated was obtained by mixing H_2S (99.7% purity from the gas cylinder) with the air stream (Fig. 2b). H₂S flow was controlled by a 5850S Brooks mass flow controller. The polluted air temperature in the biofilters ranged from 20 to 22 °C. The superficial velocity of the polluted gas in the biofilter (empty bed) ranged from $U_0 = 0.018 - 0.142 \text{ m s}^{-1}$ $(65-520 \text{ m} \text{ h}^{-1})$ corresponding to $Q=0.4-4 \text{ N} \text{ m}^3 \text{ h}^{-1}$ in flow rate. Five sampling ports were located along the column, at 20 cm intervals from the bottom, for gas sampling and pressure measurements. The H₂S concentration was measured using an Onyx 5220 device (Cosma France). To maintain the bed humidity, tap water was sprayed for 1h on the top of the column (corre-

Table	1				
Some	characteristics	of the t	hree pa	acking	materials

	Specific surface	Density (kg m ⁻³)	Maximal sorption capacity
	area (m² m ⁻⁵)		$(mg H_2 S kg^{-1} dry support)$
UP20	705	920	5
Pine bark	1120	370	110
Pozzolan	1060	1500	7

Tal



Fig. 2. (a) Experimental pilot-scale biofilters: from left to right; UP20 alone (white material), pine bark and pozzolan/UP20. (b) Schematic diagram of biofilter system for H₂S treatment.

sponding to approximatively 331), followed by 1 h stand-by. The packing materials were inoculated with washed activated sludge (1.35 g dry weight) per column twice in two weeks. The initial biomass came from the activated sludge of a wastewater treatment plant (city of Nantes, France) and was not acclimatized to treat H₂S. Apart from polluted air and UP20 material, no nutritive solution for feeding microorganisms was introduced into the biofilters.

3. Results and discussion

3.1. Effect of H₂S loading rate and pH change

The three biofilters were operated continuously for 95 days. Table 2 presents the removal capacities (RC; Eq. (1); $gm^{-3}h^{-1}$) and the removal efficiencies (RE; Eq. (2); %) for the three columns and according to the six loading rates (LR; Eq. (3); $gm^{-3}h^{-1}$) used

Table 2 Average nerfol	mances of	the three ni	lot-scale hio	urin Milters durin	ng the six ru	nning neriod	1c (O=05N	m ³ h ⁻¹ · <i>II</i> ₆ =	= 65 m h ⁻¹ · 1	(SRT = 57 c)								
and again	UP20					6 mm	Pine bark						Pozzolan/UP	20				
	1 (19 days)	2 (14 days)	3 (12 days)	4 (18 days)	5 (16 days)	6 (14 days)	1 (19 days)	2 (14 days)	3 (12 days)	4 (18 days)	5 (16 days)	6 (14 days)	1 (19 days)	2 (14 days)	3 (12 days)	4 (18 days)	5 (16 days)	6 (14 days)
LR (gm ⁻³ h ⁻¹)	0.45	0.86	1.55	3.30	5.34	8.96	0.45	0.88	1.87	3.29	4.85	9.13	0.46	1.21	2.20	3.29	5.13	9.24
$RC(gm^{-3}h^{-1})$	0.41	0.81	1.51	3.23	5.07	8.32	0.41	0.84	1.83	3.11	4.11	6.35	0.39	1.17	2.14	3.18	4.50	6.85
RE (%)	>90	>95	>97	>98	>95	>93	>00	>95	>97	>94	>86	>69	>82	>96	>97	>97	>88	>74
Hd	7.7	7.0	7.0	7.1	6.7	6.5	6.1	3.2	3.2	3.1	3.2	2.7	5.5	3.3	3.4	3.9	3.3	2.9
T (°C)	23	23	24	24	24	24	24	23	24	24	25	24	24	23	25	24	25	25

in this study. The H₂S mass loading rate was increased period by period from 0.4 to roughly $10 \text{ g m}^{-3} \text{ h}^{-1}$. For each of the six periods (2-3 weeks per period) the loading rate was kept constant. Several measurements of gas concentration from sampling ports were carried out each day of each period in order to check the condition of "steady state".

$$RC = \frac{Q}{V}(C_{\rm in} - C_{\rm out}) \tag{1}$$

$$RE = 100 \times \frac{C_{in} - C_{out}}{C_{in}}$$
(2)

$$LR = \frac{Q}{V}C_{in}$$
(3)

The change in RE versus time shows some similarity for the different packing materials and three different phases can be distinguished: (i) 30 days for the microorganisms to adapt to H₂S removal (periods 1 and 2); (ii) a maximal removal efficiency for the biofilters corresponding to periods 3 and 4 and (iii) a decrease in efficiency related to the increase in the loading rate concentration (periods 5 and 6).

After the period in which the microorganisms adapt, the three biofilters degrade more than 95% of the incoming H₂S when LR is less than $5 \text{ gm}^{-3} \text{ h}^{-1}$. The removal efficiencies obtained at the beginning of periods 2-4 are close to the values measured during all the duration of each period, which indicates the good ability of the immobilized biomass to oxidize H₂S. After 63 days of operation, LR was increased significantly to 10 g m⁻³ h⁻¹ by varying the inlet concentration. It is found that there is a noticeable decrease in the RE values for the pine bark biofilter (69%) and for the biofilter filled with the pozzolan/UP20 configuration (74%). Kim et al. [16], treating H₂S loading rates up to $13 \text{ gm}^{-3} \text{ h}^{-1}$ by the use of biomedia (from wastewater treatment plant) encapsulated by sodium alginate and polyvinyl alcohol, has obtained similar results. It thus appears that the biomass is not able to sustain such loads. In contrast, the UP20 biofilter retains a removal efficiency of more than 93% indicating a strong ability to stimulate microbial activity. This result is consistent with the results of our previously published microbial studies [7].

The removal capacity plotted as a function of the H₂S loading rates (Fig. 3) shows a linear relation up to $5 \text{ g m}^{-3} \text{ h}^{-1}$ for all three biofilters. For higher LR, the removal capacity increases at a slower rate but is of the same order for the two biofilters filled with pine bark and with the pozzolan/UP20 configuration. However, in the specific case of the biofilter filled with pozzolan/UP20, it can be concluded that such a configuration presents a benefit in comparison with pine bark: (i) UP20 stimulates the growth of bacterial activity by dissolving nutrients that flow through the pozzolan bed and (ii) the mechanical properties of pozzolan reduce the settling of the bed, which consequently should reduce the pressure drops in the biofilter. Barona et al. [17], testing four organic packing materials for H₂S removal (horse manure, sludge, soil and algae; pig manure and sawdust) have demonstrated that only pig manure and sawdust material were able to reach high removal efficiency. They obtained RE = 97% for LR = 5 g m⁻³ h⁻¹ corresponding to our results. Malhautier et al. [18], using granulated sludge from sewage treatment plant for the simultaneous biofiltration of ammonia and hydrogen sulfide, proposed very high removal efficiencies: 100% for loading rates up to $20 \text{ g H}_2 \text{ S m}^{-3} \text{ h}^{-1}$.

Fig. 4 presents the evolution of the pH in the leachate versus time for the three columns. A major contrast is observed between the UP20 biofilter and the other two. The UP20 biofilter presents a slow decrease from pH 8 to 6 throughout the six operating periods, whereas both the other biofilters drop from pH 7 to 3 during period 1 (beginning on the fifth day of H₂S treatment). A stabiliza-



Fig. 3. Removal capacity versus H₂S loading rates for the three pilot-scale biofilters.

tion period of 40 days is then observed before a new fall to pH 2.5 until the end of the experiment. Brennan et al. [19] measured a pH drop from 7-6.5 to 4.8-3.6 after 3 weeks of H₂S and methylmercaptan treatment, and after 6 months the pH decreased to reach 2. The observed rapid fall in pH could be attributed to the biotransformation of sulphite into sulphuric acid. Hence, Vincent and Hobson [20] measured a rapid acidification of the filtration material for an H₂S concentration up to 15 ppmv. In our case, the acidification occurs at a pollutant inflow concentration close to 7 ppmv. For UP20 material that has good buffering properties, the pH 8 value measured in the first days could be related to the dissolution of calcium carbonate and phosphates present in this material. This could also explain the small pH change to 6.5. Nevertheless, this acidification of the medium did not affect the removal efficiency. These results have already been observed by Yang and Allen [21], who noted that the biofiltration capacity is not affected until pH 3.2. In more acidic conditions, these authors measured a decrease in the pollutant treatment capacity.

3.2. Changes in packing material moisture content and pressure drops

The correct moisture content of a biofilter medium is also a key parameter to ensure a good performance. According to Herrygers et al. [14], the moisture content usually ranges from 40 to 60% in the biofiltration of sulphured VOC. Fig. 5 summarizes the average values of the humidity of the three pilot-scale biofilters in relation to the height of sampling and the operation time. Similar results were obtained for the biofilters filled with UP20 and pine bark. Moisture content was around 50% for UP20 at the top of the biofilter during all the operation time (70% for pine bark) while lower values were measured at the bottom of the columns. Significant decreases in moisture content with time were then measured at sampling ports 0.2 and 0.5 m, mainly due to biomass accumulation, bed compaction, clogging or/and channelling effects. Such moisture content changes are typical of the up flow gas and down flow water column. For the biofilter filled with the configuration made of two layers of pozzolan/UP20, the moisture content was around 50% at the top of the column (corresponding to the UP20 layer) but the measured values dropped in the pozzolan layer to reach roughly 15-20%. Such values correspond to the water retention capacity of pozzolan (21%). However, pozzolan showed weak variations in moisture content in the lower part of the column with time, which could indicate that this material limits drying effects and consequently preferential pathways. This result was confirmed by the measurement of pressure drops. Pressure drops in biofilters depend on both the moisture content of the packing material and the hydrodynamic conditions (superficial velocity and particle size). The Ergun equa-



Fig. 4. pH evolution in leachate versus time for the three pilot-scale biofilters.



(b) pine bark moisture content (%)



(c) pozzolan/UP20 moisture content (%)



Fig. 5. Changes in the moisture content versus operation time and along the length of each pilot-scale biofilter (from the bottom): gas flow; $Q = 0.5 \text{ N m}^3 \text{ h}^{-1}$, $U_0 = 64 \text{ m h}^{-1}$, EBRT = 57 s, sequential irrigation; 1 h aspersion ((27–391h⁻¹), 1 h stand-by).



Fig. 6. Pressure drops for the three pilot-scale biofilters: (dashed line) at the beginning, i.e., materials saturated with water; (black line): after 60 days in operating conditions.

tion [22] describes the pressure drop behaviour for a packed bed of spheres:

$$\frac{\Delta P}{H} = AU_0 + BU_0^2 \tag{4}$$

where ΔP is the pressure drop along the bed length (*H*), U_0 is the superficial velocity, and *A* and *B* are constants. Comiti and Renaud [23] proposed a model applicable in both linear and non-linear laminar flow regimes taking into account bed tortuosity and overlap between particles:

$$\frac{\Delta P}{H} = A' a_{\rm vd}^2 \tau^2 U_0 + B' a_{\rm vd} \tau^3 U_0^2 \tag{5}$$

where A' and B' are constants and a_{vd} is the dynamic surface area of particles, which can be different from the specific surface area (Table 1) if particles overlap mutually. The tortuosity (τ) is defined as:

$$\tau = \frac{L}{H}$$
(6)

where *L* is the length of the mean fluid path and *H* is the bed height. According to Mauret and Renaud [24], the model (Eq. (5)) provides a good description of pressure drops for various media such as non-consolidated beds of spheres, parallelepipedal particles, short cylinders, fibrous media and metallic foams. Eq. (5) can be rewritten as:

$$\frac{\Delta P}{HU_0} = \alpha + \beta U_0 \tag{7}$$

where α and β are the linear regression parameters allowing $a_{\rm vd}$ and τ to be calculated.

Fig. 6 shows examples of changes in pressure gradient for the three biofilters. For these measurements, the gas flow rate ranged from 0.5 to $4 \text{ N m}^3 \text{ h}^{-1} (65-520 \text{ m h}^{-1})$ and the pressure drops were measured between the sampling ports at 0.2 and 0.8 m. In this way, it is possible to compare the influence of the three packing materials (UP20, pine bark and pozzolan) on pressure drops and to take into account the presence of the 20 cm layer of UP20 topping the pozzolan bed. From the linear relation between $\Delta P/(HU_0)$ and U_0 , the hydrodynamic parameters $a_{\rm vd}$ and τ were assessed from the slope and the intercept for each packing material (Table 3). Basically, an increase of the tortuosity (τ) indicates that the contact time between the gas and the packing material increases that is favourable for the H₂S treatment. And a decrease of the dynamic surface area ($a_{\rm vd}$) that could be due to the development of the biofilm should be also better for the H₂S treatment.

At the beginning of the experiment (Fig. 6), the pressure drops measured in pine bark were 2.5-fold higher than in UP20 and 3.7-

 Table 3

 Hydrodynamic characteristics of the three packing materials: (a) at the beginning, i.e., materials saturated with water and (b) after 60 days in operating conditions

Support	lpha (Pa s m ⁻²)		eta (Pa s ² m ⁻³)		τ		$a_{\rm vd} ({\rm m}^2{\rm m}^{-3})$	
	Beginning	60 days	Beginning	60 days	Beginning	60 days	Beginning	60 days
UP20	370	342	5,730	8,440	1.78	2.26 (+27%)	420	342 (-19%)
Pine bark	608	544	14,100	15,600	3.29	3.58 (+9%)	722	617 (-15%)
Pozzolan	252	243	3,280	3,030	1.88	1.88 (-)	730	730 (-)

fold higher than in pozzolan. These results are consistent with the moisture content measurements mentioned above and can be related to the great tortuosity of the pine bark bed (τ = 3.29; see Table 3). For each biofilter, the dynamic surface area decreased in comparison with the specific surface area initially measured in dry materials (-40% for UP20, -36% for pine bark and -32% for pozzolan). After 60 days of operation, the growth of microorganisms, the development of the biofilm, the sulphur precipitation, the moisture content and the attrition of the packing material all changed the hydrodynamic properties of the biofilters (Fig. 6 and Table 3). For UP20, the pressure drop changes were the greatest. Pressure drops ranged from 8 to $217 \text{ Pa} \text{ m}^{-1}$ against 8 to $168 \text{ Pa} \text{ m}^{-1}$ at the start of the experiment. Visual observations indicated a compaction of the bed, which was confirmed by the increase in tortuosity (+27%). The decrease in the dynamic surface area (-19%) is mainly due to both the development of the biofilm and the progressive dissolution of the UP20 material. For pine bark, pressure drops varied from 15 to $388 \text{ Pa} \text{ m}^{-1}$ (from 15 to $370 \text{ Pa} \text{ m}^{-1}$ at the start of the experiment), which are comparable to the values noted by Elias et al. [4] using pig manure and sawdust $(15-460 \text{ Pa} \text{ m}^{-1})$ but lower than those of Yang and Allen [21] using compost $(0-3500 \,\mathrm{Pa}\,\mathrm{m}^{-1})$. The development of the biofilm led to a decrease in the dynamic surface area (-15%) and an increase in tortuosity (+9%). For pozzolan topped with UP20, pressure drops did not change in comparison with those measured at the beginning of the experiment (from 5 to $100 \,\mathrm{Pa}\,\mathrm{m}^{-1}$), which is comparatively lower than the pressure drops previously mentioned in conventional biofilters treating H₂S [1]. It is important to note that both τ and a_{vd} did not vary with time, which indicates that pozzolan is a good mechanical material for biofiltration. Moreover, the low moisture content in this part of the column filled with pozzolan seems to be sufficient to allow the development of a biofilm able to transform H₂S without increasing pressure drops. Consequently, pozzolan could represent the best material from a hydrodynamic point of view.

3.3. Biokinetic constants: the Michaelis-Menten type model

The removal rate of H_2S in the immobilized cell biofilter was modelled using a modified Michaelis–Menten type model [25] (with units proposed by [25] in order to compare the results with the literature data):

$$\frac{1}{R} = \frac{K_{\rm s}}{V_{\rm m}} \frac{1}{C_{\rm ln}} + \frac{1}{V_{\rm m}}$$
(8)

R: apparent removal rate $(gH_2Sm^{-3}h^{-1})$; K_s : apparent halfsaturation constant (ppmv); V_m : maximum apparent removal rate $(gH_2Sday^{-1}kg^{-1} dry material)$; C_{ln} : logarithmic mean concentration (ppmv)

$$C_{\rm ln} = \frac{C_{\rm in} - C_{\rm out}}{\ln(C_{\rm in}/C_{\rm out})}$$
(9)

$$R = \frac{Q(C_{\rm in} - C_{\rm out})}{698W[273 + T/273]}$$
(10)

where Q is the gas flow rate ($m^3 day^{-1}$); W is the dry weight of packing material (kg) and T is the temperature (°C). The kinetic constants obtained from Eq. (8) can be used to compare the characteristics and performance of various immobilized biological systems having different packing materials and configurations [26]. For H₂S treatment, the kinetic constants will depend on the microorganisms attached on the surface of packing material. Fig. 7 presents the linear relation of (1/R) versus $(1/C_{ln})$ corresponding to Eq. (8). The values of $V_{\rm m}$ and $K_{\rm s}$ obtained from this experimental study are given in Table 4. The maximum apparent removal rate was obtained for the biofilter filled with UP20 $(35 \text{ g m}^{-3} \text{ h}^{-1})$ whereas the same results were obtained for the biofilters filled with pine bark and pozzolan/UP20 (14 and 15 g m⁻³ h⁻¹, respectively). However, the K_s value determined for UP20 material was the largest (70 ppmv). Consequently, it appears that UP20 would be particularly effective in treating high concentrations of pollutant. The physical meaning of K_s corresponds to the H₂S concentration that must be treated in order to reach $V_{\rm m}/2$. In other words, a material having a large K_s value has a small affinity for H₂S. In contrast, a material having a small K_s value presents a large affinity for H₂S and the removal rate will tend toward $V_{\rm m}$ for small inlet concentrations. Consequently, both parameters $V_{\rm m}$ and $K_{\rm s}$ should not be considered separately and it is useful to compare the ratio V_m/K_s , which can give a measure of the specific activity of the microorganisms attached on the packing material for H₂S treatment (Table 4; note that K_s has been converted from ppmv to gm^{-3} in order to obtain the ratio V_m/K_s in h⁻¹). The microorganisms attached on pine bark have the same specific affinity than the microorganisms developed in pozzolan/UP20 biofilter. This specific activity is greater than those measured on UP20 alone indicating that these microorganisms can be different from those developed on both other biofilters. In conclusion, it appears that (according to the Michaelis-Menten type model): (i) at low concentrations of the pollutant, UP20 is not the most efficient material of the three tested; (ii) the configuration of two layers of pozzolan/UP20 gives better results that UP20 alone; (iii) the biofilters filled with pine bark and pozzolan/UP20 have the same efficiency for H₂S treatment. In comparison with other studies, where the operating conditions were different, it appears that the configuration of the two layers of pozzolan/UP20 is better than alginate beads and not so far from peat [22,24].



Fig. 7. 1/R versus $1/C_{ln}$ according to the Michaelis–Menten type model.

Table 4

Kinetic constants according to the Michaelis-Menten type model

Support	K _s (ppmv)	$V_{\rm m}({ m g}{ m H_2S}{ m kg^{-1}}{ m day^{-1}})$	$V_{\rm m} /({\rm g}{\rm H_2S}{\rm m^{-3}}{\rm h^{-1}})$	$V_{\rm m}K_{\rm s}$ (calculated from SI units) (h ⁻¹)
UP20	70	0.91	35	357
Pine bark	18	0.88	14	556
Pozzolan/UP20	20	0.26	15	536
Peat [25]	55	5.0	56 ^a	727
Alginate beads [27]	47	1.34	22 ^b	334

^a Estimated value from density of peat = 270 kg m^{-3} .

^b Estimated value from density of alginate beads = 400 kg m^{-3} .

4. Conclusion

The performance of three biofilters to treat H₂S at different loading rates was investigated in order to evaluate the new packing material UP20. The results from a biofilter completely filled with UP20 were critically compared with those obtained from two other biofilters, one filled with pine bark and the other with a configuration made of two layers of pozzolan/UP20. It appears that UP20 offers a real advantage for H₂S treatment at relatively high pollutant concentrations by providing both nutrients to the microbial biomass and a buffering effect. Hence, when the loading rate is significantly increased to $10 \text{ mg m}^{-3} \text{ h}^{-1}$, the UP20 biofilter retains a removal efficiency of more than 93% indicating a strong ability to stimulate microbial activity (compared to 69% for the pine bark biofilter and 74% for the biofilter filled with pozzolan/UP20). Nevertheless, at low concentrations of H₂S, UP20 is better used in combination with pozzolan as demonstrated by removal efficiency and pressure drop measurements and according to the Michaelis-Menten type model. The combined effects of pozzolan and UP20 present several advantages:

- (i) the biofilter filled with pozzolan/UP20 is able to treat the same H₂S loading rate as the biofilter filled with pine bark but with a pressure drop 3.5 times smaller;
- (ii) pozzolan is a good mechanical, chemical and physical material for biofiltration and has a long lifetime, but it is completely inert in terms of nutrient release;
- (iii) UP20 is an excellent support for biofilm development;
- (iv) UP20 provides nutrients for the development of a biofilm on pozzolan. Although the addition of nutrients would increase operating costs, it could also significantly reduce the size of the biofilter;
- (v) the UP20 layer, located on top of the pozzolan layer, could easily be replaced or fitted when required.

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